# ECE276A: Sensing & Estimation in Robotics Lecture 7: Motion and Observation Models

#### Instructor:

Nikolay Atanasov: natanasov@ucsd.edu

#### Teaching Assistants:

Qiaojun Feng: qif007@eng.ucsd.edu

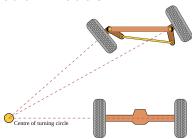
Arash Asgharivaskasi: aasghari@eng.ucsd.edu

Thai Duong: tduong@eng.ucsd.edu

Yiran Xu: y5xu@eng.ucsd.edu



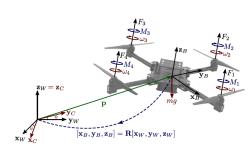
# Motion Models



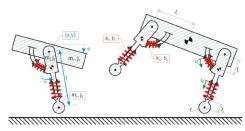
Ackermann Drive



Differential Drive



Quadrotor



Spring-loaded Gait

#### Motion Model

- A motion model is a function f(x, u, w) relating the current state x and control input u of a robot with its state change subject to motion noise w
  - ► Continuous-time:  $\dot{\mathbf{x}}(t) = f(\mathbf{x}(t), \mathbf{u}(t), \mathbf{w}(t))$
  - ▶ Discrete-time:  $\mathbf{x}_{t+1} = f(\mathbf{x}_t, \mathbf{u}_t, \mathbf{w}_t)$
- Due to the presence of motion noise, the state change  $\dot{\mathbf{x}}(t)$  or  $\mathbf{x}_{t+1}$  is a random variable and can equivalently be described by its probability density function (pdf) conditioned on  $\mathbf{x}$  and  $\mathbf{u}$ :
  - Continuous-time:  $\dot{\mathbf{x}}(t)$  has pdf  $p_f(\cdot \mid \mathbf{x}(t), \mathbf{u}(t))$
  - ▶ Discrete-time:  $\mathbf{x}_{t+1}$  has pdf  $p_f(\cdot \mid \mathbf{x}_t, \mathbf{u}_t)$

#### How is a motion model obtained?

- A motion model can be obtained using:
  - Physics-based kinematics or dynamics modeling, e.g., differential-drive model, Ackermann-drive model, quadrotor model, etc.
  - System identification or supervised learning from a dataset  $D = \{(\mathbf{x}_i, \mathbf{u}_i, \mathbf{x}_i')\}$  of system transitions
  - ► Model-based reinforcement learning, where it is inferred indirectly as the robot is learning to perform a task
- Odometry, using sensor data (e.g., wheel encoders, IMU, camera, laser) to estimate ego motion in retrospect, after the robot has moved, is an alternative to using a motion model suitable for localization and mapping but not for planning and control.

## Differential-drive Kinematic Model

- ▶ **State**:  $\mathbf{x} = (\mathbf{p}, \theta)$ , where  $\mathbf{p} = (x, y) \in \mathbb{R}^2$  is position and  $\theta \in (-\pi, \pi]$  is orientation (yaw angle)
- ▶ **Control**:  $\mathbf{u} = (v, \omega)$ , where  $v \in \mathbb{R}$  is linear velocity and  $\omega \in \mathbb{R}$  is angular velocity (yaw rate)
- ► Continuous-time model:

$$\dot{\mathbf{x}} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = f(\mathbf{x}, \mathbf{u}) := \begin{bmatrix} v \cos \theta \\ v \sin \theta \\ \omega \end{bmatrix}$$



**Discrete-time model** with time discretization  $\tau$ :

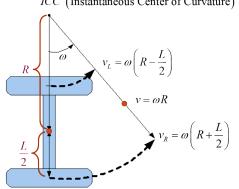
$$\mathbf{x}_{t+1} = \begin{bmatrix} x_{t+1} \\ y_{t+1} \\ \theta_{t+1} \end{bmatrix} = f(\mathbf{x}_t, \mathbf{u}_t) := \mathbf{x}_t + \tau \begin{bmatrix} v_t \operatorname{sinc}\left(\frac{\omega_t \tau}{2}\right) \operatorname{cos}\left(\theta_t + \frac{\omega_t \tau}{2}\right) \\ v_t \operatorname{sinc}\left(\frac{\omega_t \tau}{2}\right) \operatorname{sin}\left(\theta_t + \frac{\omega_t \tau}{2}\right) \end{bmatrix}$$

# Continuous-time Differential-drive Kinematic Model

- Let L be the distance between the wheels and R be the radius of rotation, i.e., the distance from the ICC to axel center.
- $\blacktriangleright$  The arc-length travelled is equal to the angle  $\theta$  times the radius R

$$\omega = \frac{\theta}{t} \qquad \qquad v = \frac{R\theta}{t} = \omega R$$

ICC (Instantaneous Center of Curvature)



$$\omega = \frac{v_R - v_L}{L}$$

$$R = \frac{L}{2} \left( \frac{v_L + v_R}{v_R - v_L} \right) = \frac{v}{\omega}$$

$$v = \frac{v_R + v_L}{2}$$

$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} v \\ 0 \end{bmatrix}$$
$$\dot{\theta} = \omega$$

# Discrete-time Differential-drive Kinematic Model

- What is the state after  $\tau := t t_0$  seconds if we apply linear velocity vand angular velocity  $\omega$ ?
- To convert the continuous-time differential-drive model to discrete time. we can solve the ordinary differential equations:

we can solve the ordinary differential equations. 
$$\theta(t) = \theta(t_0) + \int_{t_0}^t \omega ds = \theta(t_0) + \omega(t-t_0)$$

$$x(t) = x(t_0) + v \int_{t_0}^{t} \cos \theta(s) ds$$

$$= x(t_0) + \frac{v}{\omega} (\sin(\omega(t - t_0) + \theta(t_0))$$

$$\sin(\omega(t - t_0) + \theta(t_0))$$

$$\dot{x}(t) = v \cos \theta(t)$$

$$= x(t_0) + \frac{v}{\omega} \left( \sin \left( \omega(t - t_0) + \theta(t_0) \right) - \sin \theta(t_0) \right)$$

$$\dot{y}(t) = v \sin \theta(t) \Rightarrow \qquad = x(t_0) + v(t - t_0) \frac{\sin(\omega(t - t_0)/2)}{\omega(t - t_0)/2} \cos(\theta(t_0) + \omega(t - t_0)$$

$$\dot{x}(t) = v \cos \theta(t) 
\dot{y}(t) = v \sin \theta(t) \Rightarrow = x(t_0) + v(t - t_0) \frac{\sin(\omega(t - t_0)/2)}{\omega(t - t_0)/2} \cos(\theta(t_0) + \omega(t - t_0)/2) 
\dot{\theta}(t) = \omega 
y(t) = y(t_0) + v \int_{t_0}^{t} \sin \theta(s) ds$$

$$\begin{aligned} f(t) &= v \cos \theta(t) \\ f(t) &= v \sin \theta(t) \Rightarrow \\ f(t) &= v \sin \theta(t) \Rightarrow \\ f(t) &= \omega \end{aligned} = x(t_0) + v(t - t_0) \frac{\sin(\omega(t - t_0)/2)}{\omega(t - t_0)/2} \cos(\theta(t_0) + \omega(t - t_0)/2) \\ f(t) &= \omega \end{aligned}$$

$$y(t) &= y(t_0) + v \int_0^t \sin \theta(s) ds$$

 $=y(t_0)-\frac{v}{\omega}\left(\cos\theta(t_0)-\cos\left(\omega(t-t_0)+\theta(t_0)\right)\right)$ 

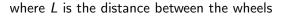
$$\begin{aligned} & (t) = v \cos \theta(t) \\ & (t) = v \sin \theta(t) \\ & (t) = v \sin \theta(t) \Rightarrow \end{aligned} = x(t_0) + \frac{v}{\omega} \left( \sin \left( \omega(t - t_0) + \theta(t_0) \right) - \sin \theta(t_0) \right) \\ & (t) = v \sin \theta(t) \Rightarrow \end{aligned} = x(t_0) + v(t - t_0) \frac{\sin(\omega(t - t_0)/2)}{\omega(t - t_0)/2} \cos(\theta(t_0) + \omega(t - t_0)/2) \\ & (t) = \omega \end{aligned}$$

$$egin{align} eta(t) &= heta(t_0) + \int_{t_0} \omega ds = heta(t_0) + \omega(t-t_0) \ & imes(t) = imes(t_0) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t_0) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t_0) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t_0) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t_0) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t_0) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) = imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \cos heta(s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t (s) ds \ & imes(t) + v \int_{t_0}^t \sin t ($$

# Ackermann-drive Kinematic Model

- **State**:  $\mathbf{x} = (\mathbf{p}, \theta)$ , where  $\mathbf{p} = (x, y) \in \mathbb{R}^2$  is position and  $\theta \in (-\pi, \pi]$  is orientation (yaw angle)
- ▶ **Control**:  $\mathbf{u} = (v, \phi)$ , where  $v \in \mathbb{R}$  is linear velocity and  $\phi \in (-\pi, \pi]$  is steering angle
- Continuous-time model:

$$\dot{\mathbf{x}} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = f(\mathbf{x}, \mathbf{u}) := \begin{bmatrix} v \cos \theta \\ v \sin \theta \\ \frac{v}{L} \tan \phi \end{bmatrix}$$



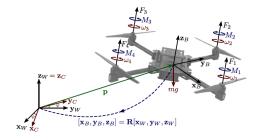
- With the definition  $\omega := \frac{v}{I} \tan \phi$ , the model is equivalent to the differential-drive model
- **Discrete-time model** with time discretization  $\tau$  and  $\omega_t := \frac{v_t}{I} \tan \phi_t$ :

$$\mathbf{x}_{t+1} = \begin{bmatrix} \mathbf{x}_{t+1} \\ \mathbf{y}_{t+1} \\ \theta_{t+1} \end{bmatrix} = f(\mathbf{x}_t, \mathbf{u}_t) := \mathbf{x}_t + \tau \begin{bmatrix} v_t \mathrm{sinc}\left(\frac{\omega_t \tau}{2}\right) \cos\left(\theta_t + \frac{\omega_t \tau}{2}\right) \\ v_t \mathrm{sinc}\left(\frac{\omega_t \tau}{2}\right) \sin\left(\theta_t + \frac{\omega_t \tau}{2}\right) \\ \omega_t \end{bmatrix}$$

# Quadrotor Dynamics Model

- ▶ **State**:  $\mathbf{x} = (\mathbf{p}, \dot{\mathbf{p}}, R, \boldsymbol{\omega})$  with position  $\mathbf{p} \in \mathbb{R}^3$ , velocity  $\dot{\mathbf{p}} \in \mathbb{R}^3$ , orientation  $R \in SO(3)$ , and body-frame rotational velocity  $\boldsymbol{\omega} \in \mathbb{R}^3$
- ▶ **Control**:  $\mathbf{u} = (\rho, \tau)$  with thrust force  $\rho \in \mathbb{R}$  and torque  $\tau \in \mathbb{R}^3$
- ▶ Continuous-time model with mass  $m \in \mathbb{R}_{>0}$ , gravitational acceleration g, moment of inertia  $J \in \mathbb{R}^{3\times3}$  and z-axis  $\mathbf{e}_3 \in \mathbb{R}^3$ :

$$\dot{\mathbf{x}} = f(\mathbf{x}, \mathbf{u}) = \begin{cases} m\ddot{\mathbf{p}} = -mg\mathbf{e}_3 + \rho R\mathbf{e}_3 \\ \dot{R} = R\left[\omega\right]_{\times} \\ J\dot{\omega} = -\omega \times J\omega + \tau \end{cases}$$



# Odometry-based Motion Model

▶ Onboard sensors (camera, lidar, encoders, imu, etc.) may be used to estimate the relative transformation:

$$_{t}\,\hat{\mathcal{T}}_{t+1}:=egin{bmatrix} {}_{t}\hat{\mathcal{R}}_{t+1} & {}_{t}\hat{\mathbf{p}}_{t+1} \ \mathbf{0}^{\top} & 1 \end{bmatrix}\in SE(3)$$

of the robot pose at time t+1 with respect to the body frame at time t

- lacktriangle Assuming a small time discretization, the estimates  $_t\hat{T}_{t+1}$  are accurate
- Let  $\mathbf{x}_0 := {}_W T_0$  be a known initial robot pose. To simplify notation, we will drop the  $\{W\}$  subscript when referring to the world frame.
- An odometry motion model estimates the robot pose  $\mathbf{x}_{t+1}$  at time t+1 (specifying the transformation from the body frame at time t+1 to the world frame) using the relative pose estimates  $_0\hat{T}_1,\ldots,_t\hat{T}_{t+1}$

# Odometry-based Motion Model

▶ Given  $\left\{\mathbf{u}_{\tau} := {}_{\tau}\hat{T}_{\tau+1} \mid \tau=0,\ldots,t\right\}$  and using the composition rule of transformations, we can estimate the robot pose at time t+1:

$$\mathbf{x}_{t+1} = T_{t+1} \approx T_{t-t} \, \hat{T}_{t+1} = \mathbf{x}_t \oplus \mathbf{u}_t =: f(\mathbf{x}_t, \mathbf{u}_t)$$

$$\approx \mathbf{x}_{t-1} \oplus \mathbf{u}_{t-1} \oplus \mathbf{u}_t \approx \ldots \approx \mathbf{x}_0 \oplus_{\tau=0}^t \mathbf{u}_{\tau} = T_0 \prod_{\tau=0}^t \tau \, \hat{T}_{\tau+1}$$

- ▶ The operation  $\oplus$  denotes composition of SE(3) elements
- ▶ The odometry estimate is "drifting", i.e., gets worse and worse over time, because the small errors in each  $_t\hat{T}_{t+1}$  are accumulated

# Observation Models



Inertial Measurement Unit



Global Positioning System



RGB Camera



2-D Lidar

#### Observation Model

An observation model is a function  $\mathbf{z} = h(\mathbf{x}, \mathbf{m}, \mathbf{v})$  relating the robot state  $\mathbf{x}$  and the surrounding environment  $\mathbf{m}$  with the sensor observation  $\mathbf{z}$  subject to measurement noise  $\mathbf{v}$ :

$$\mathbf{z}_t = h(\mathbf{x}_t, \mathbf{m}_t, \mathbf{v}_t)$$

Due to the presence of measurement noise, the observation z<sub>t</sub> is a random variable and can equivalently be described by its pdf conditioned on x<sub>t</sub> and m<sub>t</sub>:

$$\mathbf{z}_t$$
 has pdf  $p_h(\cdot \mid \mathbf{x}_t, \mathbf{m}_t)$ 

- Common sensor models:
  - ▶ Inertial: encoders, magnetometer, gyroscope, accelerometer
  - ▶ **Position model**: direct position measurements, e.g., GPS, RGBD camera, laser scanner
  - ▶ **Bearing model**: angular measurements to points in 3-D, e.g., compass, RGB camera
  - ▶ Range model: distance measurements to points in 3-D, e.g., radio received signal strength (RSS) or time-of-flight

#### **Encoders**

- A magnetic encoder consists of a rotating gear, a permanent magnet, and a sensing element
- ► The sensor has two output channels with offset phase to determine the direction of rotation
- ► A microcontroller counts the number of transitions adding or subtracting 1 (depending on the direction of rotation) to the counter
- The distance traveled by the wheel, corresponding to one tick on the encoder is:

meters per tick = 
$$\frac{\pi \times \text{(wheel diameter)}}{\text{ticks per revolution}}$$

The distance traveled during time  $\tau$  for a given encoder count z, wheel diameter d, and 360 ticks per revolution is:

$$\tau v \approx \frac{\pi dz}{360}$$

and can be used to predict position change in a differential-drive model4



# MEMS Strapdown IMU

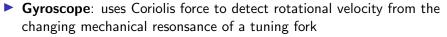
- ► **MEMS**: micro-electro-mechanical system
- IMU: inertial measurement unit:
  - triaxial accelerometer
  - triaxial gyroscope (measures angular velocity)
  - Strapdown: the IMU and the object/vehicle inertial frames are joined together/identical

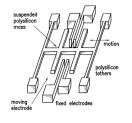


▶ A mass *m* on a spring with constant *k*. The spring displacement is prop. to the system acceleration:

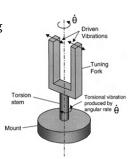
$$F = ma = kd \quad \Rightarrow \quad d = \frac{ma}{k}$$

- ▶ VLSI Fabrication: the displacement of a metal plate with mass *m* is measured with respect to another plate using capacitance
- ► Used for car airbags (if the acceleration goes above 2g, the car is hitting something!)





Surface Micromachined Accelerometer



#### IMU Observation Model

- ▶ State:  $(\mathbf{p}, \dot{\mathbf{p}}, \ddot{\mathbf{p}}, R, \boldsymbol{\omega}, \dot{\boldsymbol{\omega}}, \mathbf{b}_g, \mathbf{b}_a)$  with position  $\mathbf{p} \in \mathbb{R}^3$ , velocity  $\dot{\mathbf{p}} \in \mathbb{R}^3$ , acceleration  $\ddot{\mathbf{p}} \in \mathbb{R}^3$ , orientation  $R \in SO(3)$ , rotational velocity  $\boldsymbol{\omega} \in \mathbb{R}^3$  (body frame), and rotational acceleration  $\dot{\boldsymbol{\omega}} \in \mathbb{R}^3$  (body frame), gyroscope bias  $\mathbf{b}_g \in \mathbb{R}^3$ , accelerometer bias  $\mathbf{b}_a \in \mathbb{R}^3$
- **Extrinsic Parameters**: the IMU position  ${}_{B}\mathbf{p}_{I} \in \mathbb{R}^{3}$  and orientation  ${}_{B}R_{I} \in SO(3)$  in the body frame (assumed known or obtained via calibration)
- ▶ **Measurement**:  $(\mathbf{z}_{\omega}, \mathbf{z}_{a})$  with rotational velocity measurement  $\mathbf{z}_{\omega} \in \mathbb{R}^{3}$  and linear acceleration measurement  $\mathbf{z}_{a} \in \mathbb{R}^{3}$

#### **IMU** Observation Model

▶ Continuous-time model: with gravitational acceleration g, gyro measurement noise  $\mathbf{n}_g \in \mathbb{R}^3$ , accelerometer measurement noise  $\mathbf{n}_a \in \mathbb{R}^3$  (assumed zero-mean white Gaussian):

$$\mathbf{z}_{\omega} = {}_{B}R_{I}^{\top}\omega + \mathbf{b}_{g} + \mathbf{n}_{g}$$

$$\mathbf{z}_{a} = {}_{W}R_{I}^{\top}\left({}_{W}\ddot{\mathbf{p}}_{I} - g\mathbf{e}_{3}\right) + \mathbf{b}_{a} + \mathbf{n}_{a}$$

$$= (R {}_{B}R_{I})^{\top}\left(\frac{d}{dt^{2}}(\mathbf{p} + R {}_{B}\mathbf{p}_{I}) - g\mathbf{e}_{3}\right) + \mathbf{b}_{a} + \mathbf{n}_{a}$$

$$= {}_{B}R_{I}^{\top}\left(R^{\top}(\ddot{\mathbf{p}} - g\mathbf{e}_{3}) + [\dot{\omega}]_{\times} {}_{B}\mathbf{p}_{I} + [\omega]_{\times}^{2} {}_{B}\mathbf{p}_{I}\right) + \mathbf{b}_{a} + \mathbf{n}_{a}$$

▶ For a strapdown IMU ( ${}_BR_I = I$  and  ${}_B\mathbf{p}_I = \mathbf{0}$ ), the above simplifies to:

$$\mathbf{z}_{\omega} = \boldsymbol{\omega} + \mathbf{b}_g + \mathbf{n}_g$$
  
 $\mathbf{z}_a = R^{\top} (\ddot{\mathbf{p}} - g \mathbf{e}_3) + \mathbf{b}_a + \mathbf{n}_a$ 

▶ **Discrete-time model**: A. Mourikis and S. Roumeliotis, "A Multi-State Constraint Kalman Filter for Vision-aided Inertial Navigation"

#### Lasers



Single-beam Garmin Lidar



2-D Hokuyo Lidar

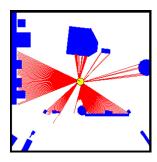


3-D Velodyne Lidar

#### LIDAR Model

- ► Lidar: Light Detection And Ranging
- Illuminates the scene with pulsed laser light and measures the return times and wavelengths of the reflected pulses
- Mirrors are used to steer the laser beam in the xy plane (and zy plane for 3D lidars)
- ▶ LIDAR rays are emitted over a set of known horizontal (azimuth) and vertical (elevation) angles  $\{\alpha_k, \epsilon_k\}$  and return range estimates  $\{r_k\}$  to obstacles in the environment  $\mathbf{m}$
- ► Example: Hokuyo URG-04LX; detectable range: 0.02 to 4m; 240° field of view with 0.36° angular resolution (666 beams); 100 ms/scan





# Laser Range-Azimuth-Elevation Model

- ▶ Consider a Lidar with position  $\mathbf{p} \in \mathbb{R}^3$  and orientation  $R \in SO(3)$  observing a point  $\mathbf{m} \in \mathbb{R}^3$  in the world frame
- ▶ The point **m** has coordinates  $\bar{\mathbf{m}} := R^{\top}(\mathbf{m} \mathbf{p})$  in the lidar frame
- ightharpoonup The lidar provides a spherical coordinate measurement of  $\bar{\mathbf{m}}$ :

$$\bar{\mathbf{m}} = R^{\top}(\mathbf{m} - \mathbf{p}) = \begin{bmatrix} r \cos \alpha \cos \epsilon \\ r \sin \alpha \cos \epsilon \\ r \sin \epsilon \end{bmatrix}$$

where r is the range,  $\alpha$  is the azimuth, and  $\epsilon$  is the elevation

- Inverse observation model: expresses the lidar state  $\mathbf{p}$ , R and environment state  $\mathbf{m}$ , in terms of the measurement  $\mathbf{z} = \begin{bmatrix} r & \alpha & \epsilon \end{bmatrix}^T$
- Inverting gives the laser range-azimuth-elevation model:

$$\mathbf{z} = \begin{bmatrix} r \\ \alpha \\ \epsilon \end{bmatrix} = \begin{bmatrix} \|\mathbf{m}\|_2 \\ \arctan\left(\bar{\mathbf{m}}_y/\bar{\mathbf{m}}_x\right) \\ \arcsin\left(\bar{\mathbf{m}}_z/\|\bar{\mathbf{m}}\|_2\right) \end{bmatrix} \qquad \bar{\mathbf{m}} = R^{\top}(\mathbf{m} - \mathbf{p})$$

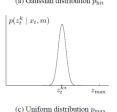
#### Laser Beam Model

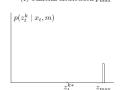
- Let  $r_t^k$  be the range measurement of beam k from pose  $\mathbf{x}_t$  in map  $\mathbf{m}$
- Let  $r_t^{k*}$  be the expected measurement and let  $r_{max}$  be the max range
- ▶ The laser beam model assumes that the **beams are independent**:

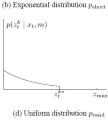
$$p_h(r_t \mid \mathbf{x}_t, \mathbf{m}) = \prod_k p(r_t^k \mid \mathbf{x}_t, \mathbf{m})$$
(a) Gaussian distribution  $p_{bit}$ 

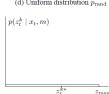
Four types of measurement noise:

- 1. Small measurement noise:  $p_{hit}$ , Gaussian
- Unexpected object: p<sub>short</sub>, Exponential
- 3. Unexplained noise: *p<sub>rand</sub>*, Uniform
- 4. No objects hit:  $p_{max}$ , Uniform









## Laser Beam Model

- ▶ Independent beam assumption:  $p_h(r_t \mid \mathbf{x}_t, \mathbf{m}) = \prod_k p(r_t^k \mid \mathbf{x}_t, \mathbf{m})$
- ► Each beam likelihood is a mixture model of four noise types:

$$p(r_t^k \mid \mathbf{x}_t, \mathbf{m}) = \alpha_1 p_{hit}(r_t^k \mid \mathbf{x}_t, \mathbf{m}) + \alpha_2 p_{short}(r_t^k \mid \mathbf{x}_t, \mathbf{m}) + \alpha_3 p_{rand}(r_t^k \mid \mathbf{x}_t, \mathbf{m}) + \alpha_4 p_{max}(r_t^k \mid \mathbf{x}_t, \mathbf{m})$$

$$\begin{aligned} p_{hit}(r_t^k \mid \mathbf{x}, \mathbf{m}) &= \begin{cases} \frac{\phi(r_t^k; r_t^{k*}, \sigma^2)}{\int_0^{r_{max}} \phi(s; r_t^{k*}, \sigma^2) ds} & \text{if } 0 \leq r_t^k \leq r_{max} \\ 0 & \text{else} \end{cases} \\ p_{short}(r_t^k \mid \mathbf{x}, \mathbf{m}) &= \begin{cases} \frac{\lambda_s e^{-\lambda_s r_t^{k*}}}{1 - e^{-\lambda_s r_t^{k*}}} & \text{if } 0 \leq r_t^k \leq r_t^{k*} \\ 0 & \text{else} \end{cases} \\ p_{rand}(r_t^k \mid \mathbf{x}, \mathbf{m}) &= \begin{cases} \frac{1}{r_{max}} & \text{if } 0 \leq r_t^k < r_{max} \\ 0 & \text{else} \end{cases} \\ p_{max}(r_t^k \mid \mathbf{x}, \mathbf{m}) &= \delta(r_t^k; r_{max}) := \begin{cases} 1 & \text{if } r_t^k = r_{max} \\ 0 & \text{else} \end{cases} \end{aligned}$$

 $z_{\text{max}}$ 

#### Cameras



Global shutter





Stereo (+ IMU)



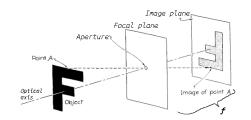
**Event-based** 

# Image Formation

- ► **Image formation model**: must trade-off physical constraints and mathematical simplicity
- ► The values of an image depend on the shape and reflectance of the scene as well as the distribution of light
- ▶ Image intensity/brightness/irradiance I(u, v) describes the energy falling onto a small patch of the imaging sensor (integrated both over the shutter interval and over a region of space) and is measured in power per unit area  $(W/m^2)$
- ► A camera uses a set of lenses to control the direction of light propagation by means of diffraction, refraction, and reflection
- ► Thin lens model: a simple geometric model of image formation that considers only <u>refraction</u>
- ▶ Pinhole model: a thin lens model in which the lens aperture is decreased to zero and all rays are forced to go through the optical center and remain undeflected (diffraction becomes dominant).

#### Pinhole Camera Model

► Focal plane: perpendicular to the optical axis with a circular aperture at the optical center



- ► Image plane: parallel to the focal plane and a distance f (focal length) in meters from the optical center
- ► The pinhole camera model is described in an **optical frame** centered at the optical center with the optical axis as the *z*-axis:
  - ightharpoonup optical frame: x = right, y = down, z = forward
  - world frame: x = forward, y = left, z = up
- ▶ Image flip: the object appears upside down on the image plane. To eliminate this effect, we can simply flip the image  $(x, y) \rightarrow (-x, -y)$ , which corresponds to placing the image plane  $\{z = -f\}$  in front of the optical center instead of behind  $\{z = f\}$ .

#### Pinhole Camera Model

- ▶ **Field of view**: the angle subtended by the spatial extend of the image plane as seen from the optical center. If s is the side of the image plane in **meters**, then the field of view is  $\theta = 2 \arctan\left(\frac{s}{2f}\right)$ .
  - ▶ For a flat image plane:  $\theta < 180^{\circ}$ .
  - For a spherical or ellipsoidal imaging surface, common in omnidirectional cameras,  $\theta$  can exceed 180°.
- ▶ Ray tracing: under assumptions of the pinhole model and Lambertian surfaces, image formation can be reduced to tracing rays from points on objects to pixels. A mathematical model associating 3-D points in the world frame to 2-D points in the image frame must account for:
  - 1. Extrinsics: world-to-camera frame transformation
  - 2. **Projection**: 3D-to-2D coordinate projection
  - 3. **Intrinsics**: scaling and translation of the image coordinate frame

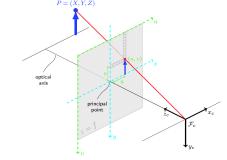
#### **Extrinsics**

- ▶ Let  $\mathbf{p} \in \mathbb{R}^3$  and  $R \in SO(3)$  be the camera position and orientation in the world frame
- ▶ Rotation from a regular to an optical frame:  ${}_{o}R_{r} := \begin{bmatrix} 0 & -1 & 0 \\ 0 & 0 & -1 \\ 1 & 0 & 0 \end{bmatrix}$
- ▶ Let  $(X_w, Y_w, Z_w)$  be the coordinates of point **m** in the world frame. The coordinates of **m** in the optical frame are then:

$$\begin{pmatrix} X_o \\ Y_o \\ Z_o \\ 1 \end{pmatrix} = \begin{bmatrix} {}_oR_r & \mathbf{0} \\ \mathbf{0}^\top & 1 \end{bmatrix} \begin{bmatrix} R & \mathbf{p} \\ \mathbf{0}^\top & 1 \end{bmatrix}^{-1} \begin{pmatrix} X_w \\ Y_w \\ Z_w \\ 1 \end{pmatrix} = \begin{bmatrix} {}_oR_rR^\top & -{}_oR_rR^\top\mathbf{p} \\ 0 & 1 \end{bmatrix} \begin{pmatrix} X_w \\ Y_w \\ Z_w \\ 1 \end{pmatrix}$$

# Projection

► The 3D-to-2D perspective projection operation relates the optical-frame coordinates  $(X_o, Y_o, Z_o)$  of point **m** to its image coordinates (x, y) using similar triangles:



$$x = f \frac{X_o}{Z_o}$$

$$y = f \frac{Y_o}{Z_o}$$

$$\begin{pmatrix} z \\ y \\ 1 \end{pmatrix} = \frac{1}{Z_o} \begin{bmatrix} f & 0 & 0 & 0 \\ 0 & f & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{pmatrix} X_o \\ Y_o \\ Z_o \\ 1 \end{pmatrix}$$
The above can be decomposed into:

The above can be decomposed into:

$$\begin{pmatrix} x \\ y \\ 1 \end{pmatrix} = \underbrace{\begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{\text{image flip: } F_f} \underbrace{\begin{bmatrix} -f & 0 & 0 \\ 0 & -f & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{\text{focal scaling: } K_f} \underbrace{\frac{1}{Z_o} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}}_{\text{canonical projection: } \pi} \begin{pmatrix} X_o \\ Y_o \\ Z_o \\ 1 \end{pmatrix}$$

#### Intrinsics

- Images are obtained in terms of pixels (u, v) with the origin of the pixel array typically in the upper-left corner of the image.
- ► The relationship between the image frame and the pixel array is specified via the following parameters:
  - $(s_u, s_v)$  [pixels/meter]: define the **scaling** from meters to pixels and the **aspect ration**  $\sigma = s_u/s_v$
  - $(c_u, c_v)$  [pixels]: coordinates of the *principal point* used to translate the image frame origin, e.g.,  $(c_u, c_v) = (320.5, 240.5)$  for a 640  $\times$  480 image
  - $ightharpoonup s_{ heta}$  [pixels/meter]: **skew factor** that scales non-rectangular pixels and is proportional to  $\cot(\alpha)$  where  $\alpha$  is the angle between the coordinate axes of the pixel array.
- ► Normalized coordinates in the image frame are converted to pixel coordinates in the pixel array using the **intrinsic parameter matrix**:

pixel scaling:  $K_s$  image flip:  $F_f$  focal scaling:  $K_f$ 

$$\begin{bmatrix}
s_{u} & s_{\theta} & c_{u} \\
0 & s_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & -1 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & -f & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & fs_{v} & c_{v} \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 & 0 & 0 \\
0 & 0 & 1
\end{bmatrix}}_{==0}
\underbrace{\begin{bmatrix}
-1 &$$

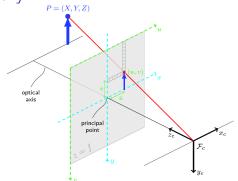
29

calibration matrix: K

# Pinhole Camera Model Summary

► Extrinsics:

$$\begin{pmatrix} X_o \\ Y_o \\ Z_o \\ 1 \end{pmatrix} = \begin{bmatrix} {}_oR_rR^\top & -{}_oR_rR^\top \mathbf{p} \\ \mathbf{0}^\top & 1 \end{bmatrix} \begin{pmatrix} X_w \\ Y_w \\ Z_w \\ 1 \end{pmatrix}$$



Projection and Intrinsics:

$$\underbrace{\begin{pmatrix} u \\ v \\ 1 \end{pmatrix}}_{\text{pixels}} = \underbrace{\begin{bmatrix} fs_u & fs_\theta & c_u \\ 0 & fs_v & c_v \\ 0 & 0 & 1 \end{bmatrix}}_{\text{calibration: } K} \underbrace{\frac{1}{Z_o} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}}_{\text{canonical projection: } \pi} \begin{pmatrix} X_o \\ Y_o \\ Z_o \\ 1 \end{pmatrix}$$

# Projective Camera Models

▶ The canonical projection function for vector  $\mathbf{x} \in \mathbb{R}^3$  is:

$$\pi(\mathbf{x}) := \frac{1}{\mathbf{e}_3^{ op} \mathbf{x}} \mathbf{x}$$

▶ Perspective projection model: the pixel coordinates  $\mathbf{z} \in \mathbb{R}^2$  of a point  $\mathbf{m} \in \mathbb{R}^3$  in the world frame observed by a camera at position  $\mathbf{p} \in \mathbb{R}^3$  with orientation  $R \in SO(3)$  and intrinsic parameters  $K \in \mathbb{R}^{3 \times 3}$  are:

$$\underline{\mathbf{z}} = PK\pi({}_{o}R_{r}R^{\top}(\mathbf{m} - \mathbf{p}))$$
  $P := \begin{bmatrix} I & \mathbf{0} \end{bmatrix} \in \mathbb{R}^{2 \times 3}$ 

- **Spherical perspective projection**: if the imaging surface is a sphere  $\mathbb{S}^2 := \{\mathbf{x} \in \mathbb{R}^3 \mid \|\mathbf{x}\| = 1\}$  (motivated by retina shapes in biological systems), we can define a spherical projection  $\pi_s(\mathbf{x}) = \frac{\mathbf{x}}{\|\mathbf{x}\|_2}$  and use it in place of  $\pi$  in the model above.
- ► Catadioptric model: uses an ellipsoidal imaging surface

#### Radial distortion

- Wide field of view camera: in addition to linear distortions described by the intrinsic parameters K, one can observe distortion along radial directions.
- ► The simplest effective **model for radial distortion**:

$$x = x_d(1 + a_1r^2 + a_2r^4)$$
  
$$y = y_d(1 + a_1r^2 + a_2r^4)$$

where  $(x_d, y_d)$  are the pixel coordinates of distorted points and  $r^2 = x_d^2 + y_d^2$  and  $a_1, a_2$  are additional parameters modeling the amount of distortion.

# **Epipolar Geometry**

- Let  $\mathbf{m} \in \mathbb{R}^3$  (world frame) be observed by two **calibrated** cameras
- ▶ Without loss of generality assume that the first camera frame coincides with the world frame. Let the position and orientation of the second camera be  $\mathbf{p} \in \mathbb{R}^3$  and  $R \in SO(3)$  (absorb  $_oR_r$  into R)
- Let  $\underline{\mathbf{z}}_1$ ,  $\underline{\mathbf{z}}_2$  be the homogeneous pixel coordinates of  $\mathbf{m}$  in the two images
- Let  $\underline{\mathbf{y}}_i := K^{-1}\underline{\mathbf{z}}_i$  be the normalized pixel coordinates so that:  $\lambda_1 \mathbf{y}_1 = \mathbf{m}, \qquad \qquad \lambda_1 = \mathbf{e}_3^{\top} \mathbf{m} = \text{unknown scale}$

$$\lambda_1 \mathbf{\underline{y}}_1 = \mathbf{m},$$
  $\lambda_1 = \mathbf{e}_3^{\mathsf{T}} \mathbf{m} = \mathsf{unknown}$  scale  $\lambda_2 \mathbf{\underline{y}}_2 = R^{\mathsf{T}} (\mathbf{m} - \mathbf{p}),$   $\lambda_2 = \mathbf{e}_3^{\mathsf{T}} R^{\mathsf{T}} (\mathbf{m} - \mathbf{p}) = \mathsf{unknown}$  scale

▶ We obtain the following relationship between the image points:

$$\lambda_1 \mathbf{y}_1 = R \lambda_2 \mathbf{y}_2 + \mathbf{p}$$

▶ To eliminate the unknown depths  $\lambda_i$ , pre-multiply by  $[\mathbf{p}]_{\times}$  and note that  $[\mathbf{p}]_{\times}$   $\mathbf{y}_1$  is perpendicular to  $\mathbf{y}_1$ :

$$\underbrace{\lambda_1 \underline{\mathbf{y}}_1^{\top} [\mathbf{p}]_{\times} \underline{\mathbf{y}}_1}_{} = \lambda_2 \underline{\mathbf{y}}_1^{\top} [\mathbf{p}]_{\times} R\underline{\mathbf{y}}_2 + \underline{\underline{\mathbf{y}}}_1^{\top} [\mathbf{p}]_{\times} \mathbf{p}$$

#### Essential Matrix

- ▶ Thus,  $\lambda_2 \mathbf{y}_1^{\top} [\mathbf{p}]_{\times} R\mathbf{y}_2 = 0$  and since  $\lambda_2 > 0$ , we arrive at the following
- ▶ **Epipolar constraint**: Consider observations  $\underline{\mathbf{y}}_1 = K_1^{-1}\underline{\mathbf{z}}_1$ ,  $\underline{\mathbf{y}}_2 = K_2^{-1}\underline{\mathbf{z}}_2$  in normalized image coordinates of the same point  $\mathbf{m}$  from two calibrated cameras with relative pose  $(R, \mathbf{p})$  of camera 2 in the frame of camera 1. Then:

$$0 = \underline{\mathbf{y}}_1^\top \left( [\mathbf{p}]_\times R \right) \underline{\mathbf{y}}_2 = \underline{\mathbf{y}}_1^\top E \underline{\mathbf{y}}_2$$
where  $E := [\mathbf{p}]$   $R \in \mathbb{R}^{3 \times 3}$  is the assential matrix

- where  $E:=[\mathbf{p}]_{\times} R \in \mathbb{R}^{3\times 3}$  is the **essential matrix**.
- **Essential matrix characterization**: a non-zero  $E \in \mathbb{R}^{3\times 3}$  is an essential matrix iff its singular value decomposition is  $E = U \operatorname{diag}(\sigma, \sigma, 0) V^T$  for some  $\sigma \geq 0$  and  $U, V \in SO(3)$
- ▶ Pose recovery from the Essential matrix: There are exactly two relative poses corresponding to a non-zero essential matrix *E*:

relative poses corresponding to a non-zero essential matrix 
$$E$$
:
$$([\mathbf{p}]_{\times}, R) = \left( UR_z \left( \frac{\pi}{2} \right) \mathbf{diag}(\sigma, \sigma, 0) U^T, UR_z^T \left( \frac{\pi}{2} \right) V^T \right)$$

$$([\mathbf{p}]_{\times}, R) = \left( UR_z \left( -\frac{\pi}{2} \right) \mathbf{diag}(\sigma, \sigma, 0) U^T, UR_z^T \left( -\frac{\pi}{2} \right) V^T \right)$$

#### Fundamental Matrix

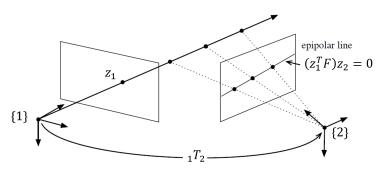
- ▶ The epipolar constraint holds even for two uncalibrated cameras
- Consider images  $\underline{\mathbf{z}}_1 = K_1\underline{\mathbf{y}}_1$  and  $\underline{\mathbf{z}}_2 = K_2\underline{\mathbf{y}}_2$  of the same point  $\mathbf{m} \in \mathbb{R}^3$  from two uncalibrated cameras with intrinsic parameter matrices  $K_1$  and  $K_2$  and relative pose  $(R, \mathbf{p})$  of camera 2 in the frame of camera 1:

$$0 = \underline{\mathbf{y}}_1^\top \left[ \mathbf{p} \right]_\times R \underline{\mathbf{y}}_2 = \underline{\mathbf{y}}_1^\top E \underline{\mathbf{y}}_2 = \underline{\mathbf{z}}_1^\top K_1^{-\top} E K_2^{-1} \underline{\mathbf{z}}_2 = \underline{\mathbf{z}}_1^\top F \underline{\mathbf{z}}_2$$

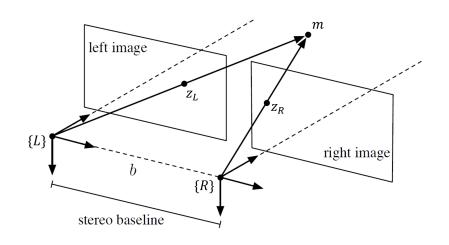
▶ The matrix  $F := K_1^{-T} [\mathbf{p}]_{\times} R K_2^{-1}$  is called the **fundamental matrix** 

# **Epipolar Line**

- ▶ If a point  $\mathbf{m} \in \mathbb{R}^3$  is observed as  $\mathbf{z}_1$  in one image and the fundamental matrix F between two camera frames is known, the epipolar constraint desribes an **epipolar line**, along which the observation  $\mathbf{z}_2$  of  $\mathbf{m}$  must lie
- ▶ The epipolar line is used to limit the search for matching points
- ➤ This is possible because the camera model is an affine transformation, i.e., a straight line in Euclidean space, projects to a straight line in image space



# Stereo Camera Model



#### Stereo Camera Model

- ► **Stereo Camera**: two perspective cameras rigidly connected to one another with a known transformation
- Unlike a single camera, a stereo camera can determine the depth of a point from a single stereo observation
- ▶ **Stereo Baseline**: the transformation between the two stereo cameras is only a displacement along the *x*-axis (optical frame) of size *b*
- ▶ The pixel coordinates  $\mathbf{z}_L, \mathbf{z}_R \in \mathbb{R}^2$  of a point  $\mathbf{m} \in \mathbb{R}^3$  in the world frame observed by a stereo camera at position  $\mathbf{p} \in \mathbb{R}^3$  and orientation  $R \in SO(3)$  with intrinsic parameters  $K \in \mathbb{R}^{3 \times 3}$  are:

$$\underline{\mathbf{z}}_L = K\pi \left( {}_oR_rR^\top (\mathbf{m} - \mathbf{p}) \right) \qquad \underline{\mathbf{z}}_R = K\pi \left( {}_oR_rR^\top (\mathbf{m} - \mathbf{p}) - b\mathbf{e}_1 \right)$$

# Stereo Camera Model

Stacking the two observations together gives the stereo camera model:

$$\begin{bmatrix} u_L \\ v_L \\ u_R \\ v_R \end{bmatrix} = \begin{bmatrix} fs_u & 0 & c_u & 0 \\ 0 & fs_v & c_v & 0 \\ fs_u & 0 & c_u & -fs_u b \\ 0 & fs_v & c_v & 0 \end{bmatrix} \frac{1}{z} \begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix} \qquad \begin{bmatrix} x \\ y \\ z \end{bmatrix} = {}_oR_rR^\top (\mathbf{m} - \mathbf{p})$$

- Because of the stereo steup, two rows of M are identical. The vertical coordinates of the two pixel observations are always the same because the epipolar lines in the stereo configuation are horizontal.
- $\triangleright$  The  $v_R$  equation may be dropped, while the  $u_R$  equation is replaced with a **disparity** measurement  $d = u_L - u_R = \frac{1}{7} f s_u b$  leading to:

$$\begin{bmatrix} u_L \\ v_L \\ d \end{bmatrix} = \begin{bmatrix} fs_u & 0 & c_u & 0 \\ 0 & fs_v & c_v & 0 \\ 0 & 0 & 0 & fs_u b \end{bmatrix} \frac{1}{z} \begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix} \qquad \begin{bmatrix} x \\ y \\ z \end{bmatrix} = {}_oR_rR^\top(\mathbf{m} - \mathbf{p})$$

# Observation Models Summary

**Position sensor**: state  $\mathbf{x} = (\mathbf{p}, R)$ , position  $\mathbf{p} \in \mathbb{R}^3$ , orientation  $R \in SO(3)$ , observed point  $\mathbf{m} \in \mathbb{R}^3$ , measurement  $\mathbf{z} \in \mathbb{R}^3$ :

$$z = h(x, m) = R^{\top}(m - p)$$

▶ Range sensor: state  $\mathbf{x} = (\mathbf{p}, R)$ , position  $\mathbf{p} \in \mathbb{R}^3$ , orientation  $R \in SO(3)$ , observed point  $\mathbf{m} \in \mathbb{R}^3$ , measurement  $z \in \mathbb{R}$ :

$$z = h(x, m) = ||R^{T}(m - p)||_{2} = ||m - p||_{2}$$

**Bearing sensor**: state  $\mathbf{x} = (\mathbf{p}, \theta)$ , position  $\mathbf{p} \in \mathbb{R}^2$ , orientation  $\theta \in (-\pi, \pi]$ , observed point  $\mathbf{m} \in \mathbb{R}^2$ , bearing  $z \in (-\pi, \pi]$ :

$$z = h(\mathbf{x}, \mathbf{m}) = \arctan\left(\frac{m_2 - p_2}{m_1 - p_1}\right) - \theta$$

**Camera sensor**: state  $\mathbf{x} = (\mathbf{p}, R)$ , position  $\mathbf{p} \in \mathbb{R}^3$ , orientation  $R \in SO(3)$ , intrinsic camera matrix  $K \in \mathbb{R}^{3 \times 3}$ , projection matrix  $P := [I, \mathbf{0}] \in \mathbb{R}^{2 \times 3}$ , observed point  $\mathbf{m} \in \mathbb{R}^3$ , pixel  $\mathbf{z} \in \mathbb{R}^2$ :

$$\mathbf{z} = h(\mathbf{x}, \mathbf{m}) = PK\pi(R^{\top}(\mathbf{m} - \mathbf{p}))$$
 projection:  $\pi(\mathbf{m}) := \frac{1}{\mathbf{e}_3^{\top}\mathbf{m}}\mathbf{m}_{\mathbf{q}}$